Design and Implementation of Expressive Footwear

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Abstract

As an outgrowth of our interest in dense wireless sensing and expressive applications of wearable computing, we have developed the world's most versatile human-computer interface for the foot. By dense wireless sensing, we mean the remote acquisition of many different parameters with a compact, autonomous sensor cluster. We have developed such a low-power sensor card to measure over 16 continuous quantities and transmit them wirelessly to a remote base station, updating all variables at 50 Hz. We have integrated a pair of these devices onto the feet of dancers and athletes, measuring continuous pressure at 3 points near the toe, dynamic pressure at the heel, bidirectional bend of the sole, height of each foot off conducting strips in the stage, angular rate of each foot about the vertical, angular position of each foot about the Earth's local magnetic field, as well as their tilt and low-G acceleration, 3-axis shock acceleration (from kicks and jumps), and position (via an integrated sonar). This paper describes the sensor and electronics systems, then outlines several projects in which we have applied these shoes for interactive dance and the capture of high-level podiatric gesture. We conclude by outlining several footwear-unrelated applications of our sensor system.

Design and Implementation of Expressive Footwear

1) Introduction

Wearable technology has long had application in musical expression. The most extreme historical example can be seen in the "one-man-band" [1], a concept that dates back well over a century, long before the dawn of electronics. In such a rig, for example as Figure 1 shows in a modern incarnation, each "instrument" is mounted for convenient access, responding to the action of a particular limb or a specific, controllable motion. Since the instruments were traditionally acoustic, each made a particular kind of sound, and the "action-to-audio" mapping was essentially static. In order to attain a timbral richness approaching that of a "band", many such instruments were scattered about the body. Despite the apparent clutter, performers could use these adornments to charm and amuse audiences with occasionally virtuosic (although often acrobatic) musical expression as they appropriately flailed away.

With the dawn of electronics, the situation evolved. Now the instruments themselves didn't have to be mounted on the performer's body, as they could be replaced by a set of electronic sensors that picked up the motion cues and controlled a remote music synthesizer. In the 1980's, the MIDI standard and digital synthesis brought these systems even further, as now a computer could be easily placed in the loop, recognizing particular motions from real-time analysis of the sensor signals and producing a more complex, dynamic, and captivating software mapping of sound onto action. This was a very liberating process, as the sensor systems freed the body from bearing the burden of

the instruments and advances in synthesis and data interpretation freed the sounds from being tied to simple causal definitions.

Most projects in such electronic musical wearables [2,3] come under the rubric of "interactive dance" [4]. An early example [5] is found in the work of composer Gordon Mumma, who adorned dancers with accelerometers to control analog synthesizers in performances of the 1960's. The well-known performance artist Laurie Anderson publicized these concepts in her shows of the 1980's [6], using active apparel like body suits adorned with percussive pickup transducers and neckties with embedded music keyboards. In the 1990's, several systems of this sort appeared. Many, such as Mark Coniglio's MIDIdancer [7], the DIEM digital dance interface [8], and the Yamaha Miburi [3] were based around placing a set of resistive bend sensors across the dancer's joints to obtain dynamic articulation. As the Miburi was a commercial product, it was packaged as a complete system, including finger controllers for each hand, a wireless interface, an embedded synthesizer, and a set of shoes with piezoelectric taps at the toe and the heel, with each shoe wired to the central beltpack transmitter.

The foot of a trained dancer is a very expressive, multimodal appendage, capable of articulating much more than simple taps. Shoe interfaces for musical performances, however, were dominated by such tap implementations [9] and, until now, haven't appreciably diversified from the toe-heel piezoelectrics.

Different applications have resulted in the adoption of other technologies for foot sensing, although essentially all of these instances concentrate on sensing only a small set of particular parameters. For example, podiatric treatment centers and product development groups at sports shoe companies use densely pixilated pressure sensors [10]

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to observe the dynamic pressure distribution on the shoe soles during walking and running. In these applications, the shoe is often tethered to a data acquisition system through a multiconductor cable. Much coarser pressure sensor arrays (e.g., sensing at only a few places) have been used in portable commercial products, such as devices to warn patients with podiatrial neuropathy about potentially damaging footfalls [11] and shoes to interactively coach a golfer on his dynamic balance [12]. A pressure-sensing overshoe has also been incorporated in "Cyberboot" [13], developed at the National Center for Supercomputing Applications (NCSA) to incorporate foot gesture into virtual reality installations. The "Fantastic Phantom Slipper" [14] was an installation that used a pressure-sensing shoe with an active IR optical system that tracked translational position across a small area, enabling users to step on animated insects that were projected onto the floor. Retrofits to jogging sneakers are now being brought to market that use inertial sensors for quantifying footfalls [15] and estimating elapsed distance (e.g., pedometry) [16].

Our "expressive footwear" device breaks these niches by using a diverse sensor suite to measure many (sixteen) different parameters at the foot, detecting essentially everything that the foot is able to do, and telemetering the data back to a remote host computer in real-time, leaving each shoe entirely untethered. Most human-computer interfaces concentrate on precisely measuring gesture expressed by the hands and fingers, devoting little, if any, attention to the feet. We have developed an interface that breaks this tradition, by measuring many parameters articulated at the foot.

2) The Sensor System and Shoe Hardware

Our instrumented shoe was initially proposed [17] in 1997, then refined [18],[19] in 1998, and perfected [20] in 1999. Figure 2 shows a diagram of the sensor system for our current shoe. Figure 3 shows a photograph of our original shoe system from 1997, grafted onto a Capezio Dansneaker, and Figure 4 shows our final design affixed to a Nike *Air Terra Kimbia* (the electronics are normally obscured by a protective Lucite cover, which was removed for this photograph). Figure 5 shows a close-up of the final version of the shoe electronics card, which can be seen to have advanced considerably beyond the initial working prototype of Figure 3.

A standard foam insole (sketched with a dotted line) is embedded with an array of tactile sensors. Two standard force-sensitive resistors (FSR's) [21] are placed at left and right in the forward region of the shoe, yielding continuous pressure there and responding to the dancer rocking the foot side-to-side. Another FSR is placed forward of the toes, at right angles to the sole so it responds to downward pressure during pointing, when the shoe is vertical. Originally, this sensor was also inside the shoe compartment, but was moved outside for more reliable operation, as its performance varied considerably across different dancers' feet. For easier integration, a more malleable "FlexiForce[®]" [22] FSR was used here (its foil cable is seen running across the side of the sole in Fig. 4). At the heel, where dynamic pressure is more relevant, we placed a strip of PVDF (polyvinylidene fluoride) [23], a piezoelectric foil that responds to changes in force [24]. Two back-to-back resistive bend sensors [25], which were placed across the middle of the insole behind the toes, measured the sole's bi-directional bend.

A strip of copper mesh adhered to the bottom of the insole acted as a pickup electrode, capacitively coupling to transmitting electrodes placed atop the stage that broadcast a constant sinusoid of 55 kHz. When the dancer is atop one of these plates, the signal received at the shoe decreases with the distance of the shoe from the plate [26], giving an indication of the height of the shoe above the stage. Another electrode (not shown in Fig. 2) is placed above the insole, right below the dancer's foot, and is connected to the local electronics ground. This breaks the symmetry [27] between the pickup electrode isolated below the insole and the local shoe electronics ground, which is now effectively coupled to the dancer's body. The dancer, in-turn is ambiently coupled to the house ground, enabling current to flow from the transmitter plates into the shoe, hence allowing the shoe system to capacitively receive the transmitted 55 kHz signal. The height of the foot is inferred from the detected signal strength.

A small $(2^1/_4" \times 3^1/_4")$ circuit board is affixed to the outside edge of the shoe atop a metal mount, containing additional sensors and electronics. In our original design, the orientation of the foot about the vertical ( ) when the foot was nearly level was obtained from an 1525 analog electromechanical compass [28], a small gimbaled magnet with quadrature position measured by a pair of Hall sensors, manufactured by the Dinsmore Instrument Corporation in Flint Michigan. This monitored the orientation of the foot relative to the ambient (Earth's) magnetic field. While the Dinsmore device was adequate for capturing slower motion during initial operation, after several hours of use the mechanics would start to fail and the gimbal would stick; the large forces and shock impulses encountered at a dancer's foot are quite hostile to any fragile devices. In subsequent versions, the electromechanical compass was thus replaced with an all-solid-

state device using permalloy bridge sensors, the Honeywell HMC2003 3-axis magnetic sensor [29], which we modified [30] for 5-volt operation and higher gain. Although this sensor was quite reliable and gave wonderful, prompt 3-axis rotational response (another degree-of-freedom above the Dinsmore), permalloy bridges can drift over time as the sensing elements loose their magnetization. Therefore, an set of "strapping" pins were provided on the shoe card; by momentarily connecting an 18-Volt source across these pins, all magnetic bridges would be subject to a brief current pulse that would magnetically saturate the permalloy, strapping it to maximum sensitivity. Over normal usage, this strapping procedure would be adequate for at least several days, if not weeks, of operation.

As spins are important gestures to detect, we mounted another rotational sensor, a compact gyroscope (a Murata GyroStar vibrating-reed device [31]), on the sensor board, aligned with the axis of the ankle. This provided a direct measurement of angular rate about the vertical, giving clear response to spins and twists.

A 2-axis, ±2 G MEMs accelerometer from Analog Devices (the ADXL202) [32] measured the tilt of the shoe with respect to the gravity vector and responded to the moderate accelerations of foot swings. Impact shocks and kicks, at higher G levels, were measured in 3-axes by a triple piezoelectric accelerometer (the ACH-04-08-05 from Measurement Specialties) [33].

A small (1 cm diameter) piezoceramic sonar receiver (e.g., the Polaroid 40KR08 [34]) detects 40 kHz pings sent from up to 4 locations around the stage. By timing the reception of their first arrival, the translational position of the shoe can be tracked. The current shoe system is able to receive pings across a distance of roughly 20 feet using our

current projectors, which are standard 1.5-cm diameter 40 kHz piezoceramic sources ganged in pairs. Additional range can be attained with more powerful emitters. With four independent projectors, at least one shoe is generally able to detect the signals from at least two projectors in our present performance configuration (see Sec. 5), fixing the dancer's position on the plane of the stage.

A "Peripheral Interface Controller" PIC16C711 microcomputer from Microchip Systems, clocked at 16 MHz, is embedded onto the shoe card to digitize all signals and produce a serial data stream, which is broadcast to a base station through a small RF transmitter, currently the "TX" series from Radiometrix [35]. Each shoe streams data at a separate frequency (418 and 433 MHz). The 20-kbit/sec peak transmitter data rate enables a full state update rate from each shoe that approaches 50 Hz. Our shoes use a helical stub antenna that protrudes behind the heel, as seen in Figs. 2-4. This enables the shoe's transmissions to easily be received across a normal stage; we have used them successfully beyond 100 feet from their base stations, but this performance depends, of course, on the local RF environment. Although these transmitters output just under a milliwatt, they are still too strong for FCC regulations, which run 2-3 μW in these bands (likewise, emission at 418 MHz is limited to brief duration); the corresponding European limits, for which these transmitters were designed, are much more liberal. Such rules certainly restrict the carefree operation of our present system. As outlined in the last section of this paper, we are currently developing higher-bandwidth, channel-shared communications hardware that will allow for the legal operation of multiple embedded transmitters that meet our requirements.

All onboard shoe electronics drain about 50 mA at 5 volts. The original shoe system used an onboard $^1/_2$ AA-size 6.2 Volt lithium camera battery, which provided for up to a few hours of useful life. After the first model, however, we moved to an off-card 9-Volt alkaline battery, which provides for at least a half-day of very stable continuous performance. Although the operation could be extended significantly by substituting a switching regulator for the on-card series regulator or only powering the compass module (which consumes nearly half of the board's current) during its readout [36], this battery life span was already ample for our performance applications, so the additional design complication wasn't warranted.

This shoe system is much easier to work with than most other types of wearable interfaces. One only needs to put the shoes on and flip their power switches; there are no connectors, tethers, cables, harnesses, etc. to worry about. Although some of the sensor systems (e.g., the sonar) could be well implemented at other locations on the body, having all devices concentrated at the shoes greatly simplified the setup. Many dancers have worked with this system and have encountered few, if any problems with the mechanics and location of the electronics module or antenna (out of the two, the antenna proved the most restrictive, as it could limit ankle motion). It should be noted, however, that all of our dancers worked in more of a freeform, interpretive and improvisational modern genre, as opposed to traditional styles like tap and ballet, which may involve more constraints. With more engineering (e.g., going to an embedded loop antenna and distributing the electronics throughout the shoe), the system can be made much more innocuous. In addition, the current device is to a large extent hardwired into a particular

shoe; additional design can make such a system modular, perhaps clipping onto a shoe with an adjustable insole that is adaptable across a wide range of foot sizes.

3) Electronics, Base Stations, and System Integration

This section describes the electronics design and integration of the shoe system components. More detail can be found in Ref. [30]. Fig. 6 shows a block diagram of the electronics for the embedded shoe system. All sensors, except for the sonar and the two low-G accelerometer channels, produce analog voltages, which are conditioned, routed to CMOS multiplexers, then digitized by the 8-bit converter onboard the PIC.

Signal conditioning for the FSR sensors is simply an emitter follower; as no voltage gain is required, this allows the FSR's series gain-setting resistor to become as large as needed to provide adequate response to toe pressure, while presenting a low impedance to the PIC's A/D inputs. Likewise, the PVDF signals are buffered by a Junction Field-Effect Transistor (JFET) source follower, enabling the PVDF shunt resistance (which limits the low-frequency bandwidth) to be set at 40 M . The back-to-back bend sensors are fed through a differential amplifier to give bi-directional response. The capacitive pickup signal is first conditioned by a passive LC bandpass filter tuned to the 55 kHz transmitter (rejecting ambient background at other frequencies), then fed through a gain block and half-wave envelope detector that extracts the positive amplitude of the received signal. The three shock accelerometer signals are amplified, then time-stretched with a similar half-wave envelope detector, allowing them to be reliably digitized by the PIC across its data acquisition cycle. Although this loses polarity information, the raw accelerometer signals are too narrow for the PIC to reliably detect at

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its 50 Hz sampling updates. The signals coming directly from the Murata gyroscope are perfectly within the 0-5 Volt digitization range without further conditioning, as are the 3 signals output from the Honeywell compass after it has been custom modified, as mentioned earlier. In addition, the regulated 3-volt supply used by the RF transmitter module is digitized by the PIC and transmitted with each data set, as it is used to continuously monitor the 5-volt supply (the 3-volt input will appear to grow as the 5-volt supply, which is used as the A/D reference, droops).

The latest version of the shoe electronics card has two 8-channel analog multiplexers; together with the 4 analog inputs already available on the PIC, this gives 18 available analog channels. Since the shoe system only uses 14 of these, the extra 4 inputs are brought to a header, where they are available for other devices (e.g., useful when the card is embedded in systems other than the shoe, as mentioned in Section 6).

The two low-G accelerometer outputs are digital 1 kHz pulse trains, with the duty-cycle of each pulse corresponding to the detected acceleration along the respective axis. They are thus input directly to a pair of PIC digital inputs. After the PIC digitizes the analog data, it software-times the accelerometer pulse-widths, retaining 8 bits of resolution.

The signal from the sonar receiver is likewise first amplified (as the piezoceramic head is already highly resonant, there's no bandpass filtering), then routed through a half-wave envelope detector and sent to a discriminator with adjustable threshold (setting the sonar sensitivity). The discriminator output is applied to a PIC digital input that can generate an interrupt when the discriminator goes high, executing a tight segment of code that starts the PIC's timer and sets a "sonar received" flag. When the PIC is about to

transmit the byte in the serial data record dedicated to the sonar, it checks this flag to see if a ping was received, and if so, it sends the timer value (otherwise it sends zero). This parameter is thus the latency between the time when the ping was received and the time when the sonar byte was transmit. Making the sonar threshold manually adjustable allows the user to set the tradeoff between sonar sensitivity (e.g. range of operation) and any 40 kHz background noise. Most of this noise is caused when the dancer lands hard from a jump or stomps a foot; as the accelerometers also detect this state nicely, any such spurious sonar spikes that coincidentally occur can be removed in the basestation or subsequent PC software.

The primary 5-volt supply for the shoe hardware is conditioned by a low-dropout series regulator that produces a battery-low gate, tripped when the battery drops below 5.3 Volts. This gate is also read by the PIC and encoded into its data transmission.

Figure 7 is a block diagram for the base station. It is much simpler, mainly consisting of a PIC 16C73 microcomputer (during the hardware design cycle, it was the smallest PIC with hardware serial ports) that receives serial input from a Radiometrix RX-series RF receiver (picking up transmissions from the shoe) and sends serial output to a RS-232 driver (for communicating with a PC serial port).

In order to provide an appropriately zero-balanced RF serial stream, the shoe's PIC uses a very simple, brute-force variation of Manchester encoding, where it first sends all data bytes for a full record of sensor values, then sends their binary compliments. Additionally, by comparing each data byte in a record with its transmitted compliment, RF reception errors are detected, and individual bad bytes are "failed" and ignored, keeping the rest of the record intact. In order to enable the base station to quickly

synchronize to the shoe's data cycle, the first byte in a record is marked with a unique code (either 254 or 255, depending on the battery-low gate), which isn't allowed to appear in subsequent values.

Figure 8 shows a high-level block diagram of the entire expressive footwear system. In the current rendition, two base stations are needed, one for each shoe. Each base station listens for its shoe at a different RF frequency (as mentioned, 418 or 433 MHz). One of the base stations, deemed the "master", also has an onboard 55 kHz sinewave generator and driver for the electric field transmitter plates (detectable by both shoes). The master's PIC additionally generates 4 gates for the sonar pingers, each of which produce a few-millisecond burst of 40 kHz ultrasound when triggered. The master pulses a sonar gate every tenth of a second, going round robin through all connected pingers. The master's PIC uses its timer to measure the interval between sending the ping and receiving a valid sonar-detected byte from the shoe. The value of the sonar byte sent from the shoe (containing the latency in the shoe) is then subtracted from the value of the master's timer (containing the acoustic transit time plus shoe latency), resulting in the amount of time it took the ping to reach the shoe, hence the distance of the shoe from the pinger. This sonar system works satisfactorily, providing 8 bits of position resolution across a 30-foot range. As seen in Figure 8, a pulse from the master synchronizes the slave base station when the master sends each ping. This pulse interrupts the slave's PIC to start its timer, enabling the same sonar algorithm to work there. The master and slave base stations keep track of which sonar head was the last to ping, sending that address along to the host PC with every data record.

The current system produces a pair of 19.2 kBaud serial streams from master and slave base stations that are combined in the analysis and content software running on the host PC. The 50 Hz state-update cycle is primarily limited by the 20 kbit/sec RF data rate, which is at the edge of capability for the Radiometrix transmitter and receiver modules that we are currently using. A more efficient zero-balancing scheme would likewise speed up the effective data rate (to within a factor of two). The data interpretation algorithm running on the host PC provides another layer of error protection by ignoring any spurious "spikes" on most sensor signals (e.g., data that abruptly jumps from the baseline to a significant value then returns directly to the baseline on the subsequent sample). This introduces an intrinsic delay of one 20 ms data cycle.

4) System Performance

The data stream produced by the shoe system is very rich, providing much detail on the gait and foot dynamics. This can be seen in the sample data plotted in Figure 9, which shows a 12-second "stripchart" excerpt of the raw outputs from all 16 sensor subsystems on a single instrumented Nike sneaker, as wirelessly received at the host PC. At the beginning of the data sample, the user walked towards the sonar head, starting roughly 15 feet distant and ending up a foot or two away after 6 seconds. This is clearly seen in the sonar range data, plotted at top left, where individual footfalls create a stairstep structure. In this example, only one sonar projector was used, pinging at 10 Hz. The regular signature of the gait can be seen in the pressure and bend signals, plotted below the sonar. The difference between the FSR and PVDF response is obvious, the

former providing steady-state pressures as the toes bear down, while the latter giving a differential signal that responds to the attack and release of the heel. The FSR signal decreases with increasing pressure; as noted in Fig. 9, the FSR's are biased to be slightly insensitive for a conventional person's walk, yielding more range for a dancer up on their toes, where the pressures are higher.

After about 7 seconds, the walking stops, and the foot is moved about more wildly, as can be noted in the drop in the consistency of the pressure signals. At roughly 11 seconds, the foot is rotated perpendicular to the floor, and the wearer presses the front of the shoe against the ground, as seen in the tip pressure plotted in the second graph at left (as this action is very deliberate and the data very clean, it's a good candidate to use for triggering important events). The sole bending is also seen to be unipolar and modest through most of the test, as expected, since jogging sneaker soles aren't easily reverse-bent (the exception is near the end of the test, when the foot was rotated and pushed against the floor).

At 6 seconds, two steps were made atop the 55 kHz electric field transmitter plate, as clearly seen in the "capacitive height" signal, which gives an extremely simple and reliable signature.

The gait dynamics also leave some traces in the twist gyro (bottom left) and low-G accelerometer signals (top right), which can be seen to jump more in the latter part of this test, when the foot was moved about more wildly (both of these channels have still additional headroom to respond to a dancer's very fast twists and foot swings). Some muted traces of gait can also be seen in the shock accelerometer traces (middle right), but 3 sets of spikes, corresponding to foot stomps, stand out clearly after 8 seconds, primarily

in the second and third sensor axes. The directional difference in the foot strike acceleration is evident from the balance between amplitudes. The low-G accelerometer is relatively insensitive to impacts, as they are too transient. If it responds at all, it tends to produce a very narrow and modest spike (as seen in this data), which the analysis software rejects as noise. As designed, the accelerometers are complimentary systems: the low-G channels indeed pick up foot swings and tilts, while the high-G sensors nicely detect the shocks.

The magnetic field ("compass") signals, at lower right, are likewise seen to follow the gait, gyrating as the foot pitches cyclically during walking or giving different response when the foot rotates during a turn, twist, or swing. At the end of the test, Compasses 1 and 2 show the foot pitching up when the tip was pressed against the floor.

5) Dance Applications

Figure 10 is a set of photographs illustrating all of the artistic projects and collaborations in which we've used the shoe system, placed in chronological order, left-to-right. Since we were then developing our system, the first few employed dance and athletic talent resident in the MIT student and affiliate community. By 1999, our system was sufficiently robust and advanced to engage professional choreographers and performers for extended public shows. Video clips for all of our expressive footwear projects are available online [37]. All of the software that mapped sensor values into sound ran on standard PC's and laptops, driving external synthesizers via ROGUS [38], a set of C++ libraries written at the Media Lab to handle MIDI.

Our musical mappings are essentially "direct manipulation" [39], where sonic events are tied to sets of simple gestures under direct control of the dancer (as opposed to trying to garner more sophisticated gesture from a higher-level analysis of the data, which, although interesting from a research viewpoint, can risk removing some of the dancer's immediate control). This strategy gives improvisational dancers a "palette" of action-sound rules and relationships that they can exploit to evolve a compelling performance after practicing with the system.

As our prototype shoe (Fig. 2) was designed to be exhibited at the first IEEE conference on Wearable Computing [17] in October 1997, it was pressed into actual stage performance a few days later at the subsequent "Beauty and the Bits" event [40], the world's first wearable computing fashion show, held at the MIT Media Laboratory. Because only one base station had been constructed, this mapping used only a single shoe. All subsystems, excepting the sonar, provided usable data. As it was intended for a brief on-stage walkthrough, the mapping, as described below, was very simple and literal; easily mastered, although very limited in scope.

The music itself consisted of three voices: a drum voice, a bass voice, and a melody voice. The drum voice ran steadily throughout the whole piece and gave a rough "techno" feel to the music, fitting the mood of the fashion show. The volume of the bass drum and the bass voice were controlled by the   (pitch) tilt accelerometer, and the electric field height sensor controlled the volume of the other drum instruments. The tempo was adjusted slightly by the bend sensor. The bass voice and melody voices were switched on and off in various combinations as impulses were detected by the shock accelerometer. The bass voice produced a harmony effect, and the specific harmony was

selected by rotating the shoe in   (yaw). The bass voice was articulated by changing its octave upon detecting impulses from the rear PVDF sensor. The melody voice played harmonizing tones in upper registers; the range of the melody voice was controlled by the front pressure sensors. Panning and flanging of both voices were controlled by the detected compass direction. Also attached to the high-G accelerometer was an explosion sound, triggered by heavy stomps and kicks. Finally, a panning wind sound was produced with quick   rotations, as detected by the twist gyro. An MIT student dancer, Yuying Chen, practiced with these mappings, and performed at the Fashion Show (Fig. 10, top left).

The next application used athletic shoes, and was built around the Nike's of Fig. 3. This mapping has no pedestrian rhythm, but is entirely freeform, triggering and modifying simple sounds in accordance with the dancer's gesture, hence providing the audience with a more direct causal link. We tied random melodic notes to toe and heel pressure, and the bend of the sole selected a harmony chord that was changed in volume in accordance with the pitch tilt ( ) of the shoe; roll tilt ( ) faded up an additional harmony chord. The height of the shoe above an electric field transmitter embedded in the carpet dictated the volume of the bass pedalpoint notes (they increased in volume as the shoe approached the floor). A fast movement or stomp, as detected by the shock accelerometers, introduced percussive sounds, and fast twists, as indicated by the rate gyro, introduced a stream of random piano notes. Our performer here (Fig. 10, second-left) was another MIT semi-professional dancer, this time Mia Keinanen from the Media Lab's Gesture and Narrative Language Group.

Our next mapping was with an athlete, Brian Clarkson, a trained gymnast and student in the Media Lab's Vision and Modeling Group. The performance took place during the Wearable Computing Fashion Show at Nicograph 98 in Tokyo. Here, we went back to having the performer's actions embellish a background pedestrian music sequence, as in our original example. Notes were likewise tied to toe pressures and transposed with bend. Glissandos were attached to spins and tilts, sharp sonic transients to jumps, and panning/crossfading to the compass. When the performer approached the portion of the stage where the electric field sensor was embedded, a percussion track faded up. Additional effects were introduced specifically for Brian's gymnastic style; a sharp blast of noise for very fast spins and detection (via the low-G accelerometers) of handstands, at which point a drumroll would begin, finishing in a loud crescendo when he landed.

At this point, the shoe system was reliable enough to use in performance with dance professionals, thus we enlisted the collaboration of Byron Suber, a choreographer from Cornell University's Dance Department. Taking the gymnast's mapping as a starting point, we worked with Byron to make it dance-relevant, going through the musical response of each sensor, one by one. This resulted in a complex, yet very controllable demonstration piece that again dispensed with the background sequence and enabled the dancer to launch and modify a variety of sounds, using all of the sensor systems simultaneously. In this mapping, the right/left toes and heels produced various melodic tones in an assigned harmony (pressure sensor response from both feet must be present for these tones, thus insuring that they are both on the ground). Bend of the sole transposed these toe melodies by an octave, up or down depending on the bend direction,

and pressure at the toe tip sensors triggered cymbal crashes. The gyro picked up twirls, again launching a cascading glissando (and burst of white noise for very fast right-spins). The shock sensors launched orchestra hits, and the left foot's shock also turned off all notes and changed the harmony played by the toes. Forward pitch tilt ( ) launched "sparkling" notes for the left foot and a digital pad in the right foot, while sideways roll ( ) tilt would adjust the octave ranges of sounds controlled by the corresponding pitch tilt. This version of the system had functioning sonar; as the shoes approached the single sonar pinger used in this mapping, a cymbal/snare rhythm would start, growing louder with the dancer's approach. If the dancer stepped on the electric field transmitter, all sounds would stop, and a droning chord would fade up, increasing in volume as the foot was lifted away from the electrode (different sound on each foot), with the chord voicing changing as the foot was rotated (as derived from the compass signal).

This mapping was debuted in a live demonstration at the International Dance and Technology Conference 99 in Tempe Arizona [19] and tried by many dancers (e.g., Fig. 10 shows Boston dancer Dawn Kramer performing with it for a television newscast). The sonic palate was rich and controllable, allowing a dancer to acclimate to it within an hour or so of practice, as it gave both complex, causal and appropriate response to their motion. It also succeeded outside of the dance community; for example, we worked with a juggler (lower left of Fig. 10), who used it to sonically embellish his mime/juggling routine in scores of regular public performances at the 1999 Tokyo Toy Fair.

Our last mapping was far more complex. It was developed for a performance and demonstration at the July 1999 American Dance Festival with a pair of dancers (one each with one active shoe; lower middle of Fig. 10) choreographed by Byron Suber and

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refined further for New York choreographer/dancer Mark Haim's solo performance (lower right of Fig. 10) during the Sens*bles conference at MIT's Kresge Auditorium in October 1999. The stage setup used in this performance is shown in Figure 11. The sonar system was now fully operational, hence all four projectors were deployed at the corners of the square capacitive transmit plate (they can be seen in the Figure 10 photo of Mark Haim). The resultant tracking was used to zone the stage up into discrete regions, as labeled. This quantization was used to generate a dynamic musical mapping, where the musical mode would depend on the regions in which the dancer was located and/or had visited.

By default, there is no quiescent background sound over this mapping. The dancer(s), however, can select a looped music sample to start playing by staying relatively stable for several seconds in regions A31 or A13, with the left foot facing the center square. There are five samples of different musical excerpts in all (30-second loops, ranging from Cajun music to classical), and these are selected by the region and range at which the trigger occurred. The sample will continue playing until the dancer toe-taps (i.e., points the front of the shoe down and presses) on the left foot. In contrast, toe tapping at any time on the right foot plays a brief portion (e.g., 5 seconds) of a minimalist MIDI sequence written by Cornell composer David Borden, each of which has 3 parts that the dancers can add and subtract with additional toe tapping. When a shoe is lifted and tilted (or swung), continuous audio effects will be proportionally added to a voice in the sequence or to the music sample (e.g., filtering, flanging, reverb, crossfading, or vibrato, depending on what's currently playing). Both angles (,) of tilt are used, allowing one shoe to control the mix of two different effects. The pressure sensors in the

sole again sound notes (bass on the heel, melody on the toes), except when a music sample is playing, at which point they trigger soft percussive sounds. These (together with the backing sequence, if appropriate) will transpose up and down with bend of the shoe. If a dancer is in zones A11 or A33, the sole's pressure sensors will play different pitched speech phrases pronounced by a computer-generated voice, allowing the dancer to put musical sentences together with their movement. These phonemes are also transposed by the sole's bend, and effects are similarly introduced with tilt. Throughout the dance, different sonic events are tied to the shock accelerometer signals (e.g., jumps, leaps) and rate gyro, as in the previous mapping. The shock sensor response is also processed to determine the intensity of the dancer's activity. If it's relatively smooth, the shock sounds are distinctive, but not dominant. As the dancer's motion becomes more vigorous and sustained, the shock sounds become progressively more intense. When a shoe enters the electric field transmitter at stage center, the same effect is produced as in the previous mapping; e.g., any background notes or samples are silenced, and orientation-dependent drones are produced. Fast foot swings in this region are detected by the low-G accelerometer, and launch swooshing sounds. Every time a dancer enters and leaves the central electric field region, the voices playing the notes triggered by the insole pressure sensors change (there are 7 voice loads defined, which cycle round-robin with each visit to the transmitter pad).

This mapping has advanced the shoe system well beyond the "demo" stage. It has sufficient depth and variation for professional dancers to work with in many different ways, entertaining an audience throughout an extended performance.

In an entirely different project [41] using the prototype shoes, real-time classification algorithms have been developed that detect certain dance styles from the shoe data stream; e.g., discriminating between a waltz and a tango. After exposing the analysis to several seconds of the real-time dance data, the appropriate musical accompaniment would fade up once the decision was completed. As the data streaming from the shoe system provides a rich description of poditrial activity, this project represents only the first step in a very promising trajectory of applying more sophisticated analysis to the data stream for extracting higher-level features, useful in dance and sports training or podiatric therapy.

6) Other Applications

Once we had developed and demonstrated the compact, wireless sensor circuit card of Fig. 5, several other research groups at the Media Lab and in its sponsor community began to inquire about embedding it into devices and places far different from a dance shoe. These were applications where inertial, positional, and tactile cues could open entirely new applications; for example, interactive kites [42], new kinds of digital "tape measures" [43] and sensate biker's helmets [44]. Our closest and most unusual collaborations, however, have been with Bruce Blumberg's Synthetic Characters group [45], which produced the items shown in Fig. 12. The left photograph shows the wireless "chicken" interface used for the *SWAMPED!* installation [46] exhibited at SIGGRAPH 98. This was a toy (completed at right) with a shoe card embedded in its center (as seen in the unclothed prototype at middle), which controlled an animated chicken agent (seen on the screen at left). The shoe card measured the inertial motion

queues and different pressures, bends, and twists around the doll, wirelessly transmitting these parameters back to a host computer, where a gesture-recognition algorithm [47] was run on the resultant data and appropriately instructed the animated agent.

The right photograph in Fig. 12 shows an evolution of our shoe sensor concept into a different form factor: a wireless, 6-axis inertial measurement unit (IMU) that fits inside a common bread bun, complete with microcomputer, RF transmitter, loop antenna, and a battery that lasts for at least 2 days of continuous operation while streaming data at 65 Hz. A pair of these devices [48] was built for the *Void** installation [49] shown at SIGGRAPH 99. In this exhibit, a user could control one of three semi-autonomous virtual characters, causing them to dance. Drawing inspiration from Charlie Chaplin's famous "buns and forks" scene in *The Gold Rush* [50], we created a pair of input devices whose outer casings were two bread rolls, each with a fork stuck near the end, thereby mimicking a pair of legs. The IMU was placed inside the buns. A variety of gestures (kicks, twirls, etc) were recognized (using a similar gesture-recognition algorithm to that in *SWAMPED!*) and used as controls for the virtual characters. These buns also transmitted a coded, low-frequency RF signal that enabled them to be identified when placed near capacitive receivers embedded in the table top, under a set of dinner plates.

7) Conclusions and Future Directions

After several development cycles and lessons learned from experience with performers and athletes, as chronicled in this article, we have developed the world's most versatile human-computer interface for the foot. Although our device is very usable and quite robust, additional design can make the electronics less obtrusive and enable an easy

retrofit to shoes of different sizes (our final shoes were a men's size 10, but spanned a much wider range of feet by adding or subtracting layers of socks). Simple power management and regulator optimization can extend the continuous battery life significantly beyond its current half-day span.

The RF solution taken here, devoting one fixed frequency to streaming data from a particular shoe (see Fig. 8), is inefficient and often illegal operation in several parts of the world. Rather than devoting a separate base station to each shoe, a superior strategy is shown in Fig. 13, where a higher-bandwidth channel-sharing scheme (e.g., CDMA or TDMA) is used to address several such wireless sensor packages. Although this involves significantly more complication in the RF hardware and data management/handshaking schemes, it scales much better, allowing us to more easily instrument a full ensemble of dancers and/or place many discrete wireless sensor packages around a dancer's body to access additional gestures beyond the feet. Commercial packages are now making an appearance that have the potential of solving this problem; e.g., the single-chip [51] Bluetooth [52] transceivers. Although appealing to the many consumer applications for which they are being developed, Bluetooth devices are limited to 7 nodes per base station and devote considerable overhead to dynamic network management; a capability that's not necessary (and potentially detrimental) for performance applications of the sort that are described in this paper. We are thus developing a new system [53], diagrammed in Fig. 13, that uses a static network topology that can be *a priori* programmed into a "heavy" basestation, which communicates with a set of lightweight, low-power, fast TDMA transceivers at each sensor package.

Although placing so many sensors at the feet was novel and technically challenging, it was an adjustment for many modern dancers who were used to gesturing more equitably across their entire body. By contrast, most current interactive dance systems are based around video tracking (e.g., [54]) which *only* monitors the body proper and doesn't adequately address the feet. After some hours of practice, our dancers acclimated and learned to direct most gestures through their feet, where they would get appropriate musical response.

This system presents a different environment from a standard tap shoe, which produces its output only when in contact with the floor. Although our system is somewhat slow for precise tap performance (limited by the 50 Hz state update rate coupled with any processing delay incurred at the host PC), the foot dynamics were continuously measured by the inertial, tracking, and tactile systems when elevated up off the stage, enabling other expressive degrees of freedom.

We have barely begun to subject the rich, descriptive data streaming from our shoe system to significant gestural analysis, an area promising to bear fruit for automated dance training, sports coaching, podiatric therapy, or biomotion research. Such data acquisition systems also promise to open new vistas into professional sports broadcast, especially in the upcoming era of digital television. Exploiting similar dense sensor packages, data can stream directly from the figure skater's blades or boxer's glove to the viewer's entertainment system, where it is mapped onto different information representations, potentially including parametrically adjustable musical mappings, like those explored here.

This shoe music system blends music composition with dance, as aptly articulated by Merce Cunningham [4]. Since our recent mappings give performers access to a complicated musical palette linked to their motion, virtuosity with such devices logically requires some level of musical talent. It is thus no coincidence that dancers who are also adept musicians seem to do the best work with our shoe system.

8) Acknowledgements

9) References

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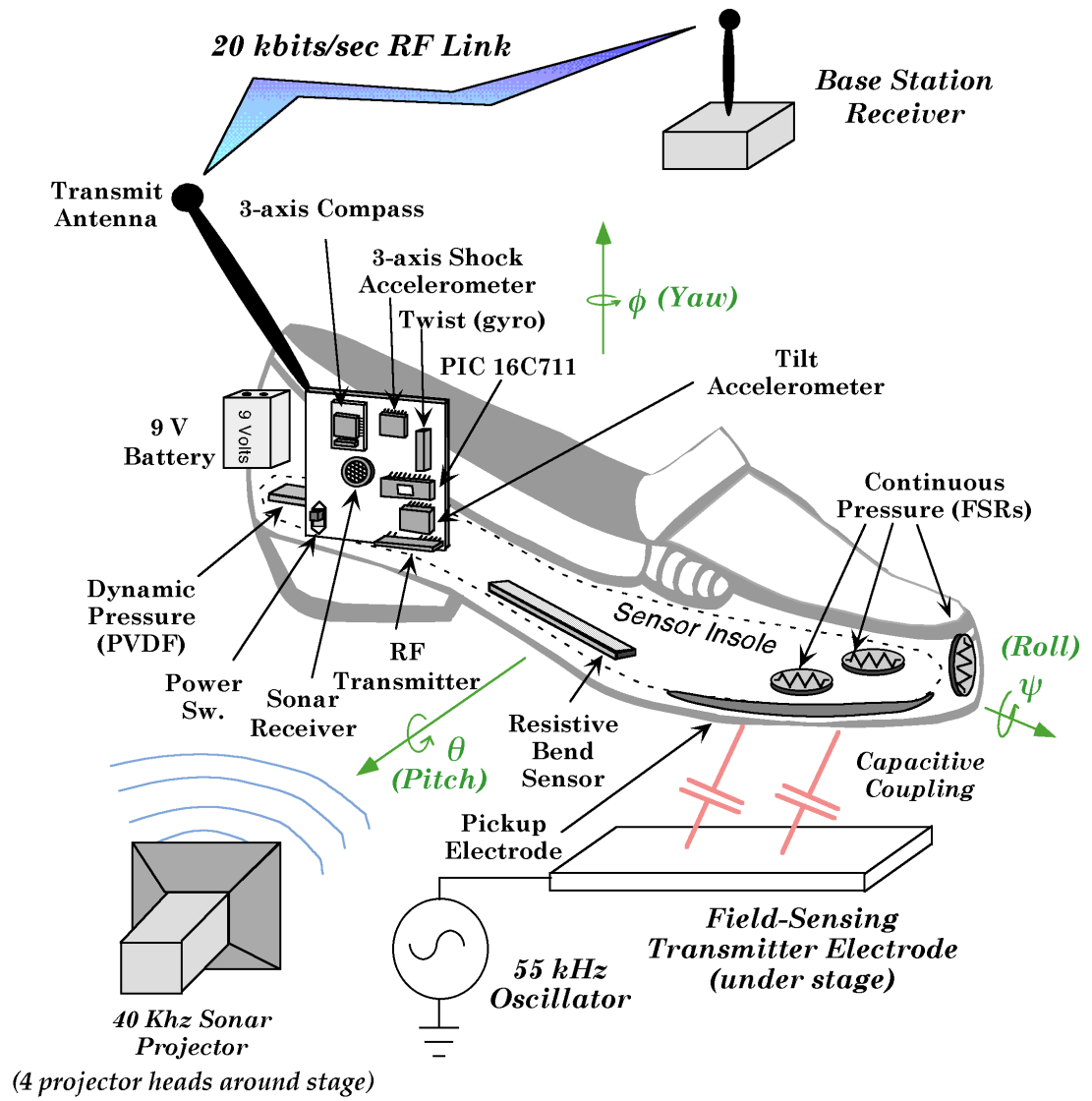
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Figures and Captions:

Figure 1: A simple one-man-marching band setup: an example of pre-electronics wearable technology for musical expression

20 kbits/sec RF Link

Base Station Receiver

Transmit Antenna

3-axis Compass

3-axis Shock Accelerometer

Twist (gyro)

PIC 16C711

ϕ *(Yaw)*

Tilt Accelerometer

9 V Battery

9 Volts

Continuous Pressure (FSRs)

Dynamic Pressure (PVDF)

Sensor Insole

(Roll)

ψ

Power Sw.

Sonar Receiver

RF Transmitter

Resistive Bend Sensor

θ *(Pitch)*

Pickup Electrode

Capacitive Coupling

40 Khz Sonar Projector

(4 projector heads around stage)

55 kHz Oscillator

Field-Sensing Transmitter Electrode (under stage)

Figure 2: Functional Diagram of the Expressive Footwear Electronics and Sensor Suite

Figure 3: The original working prototype shoe
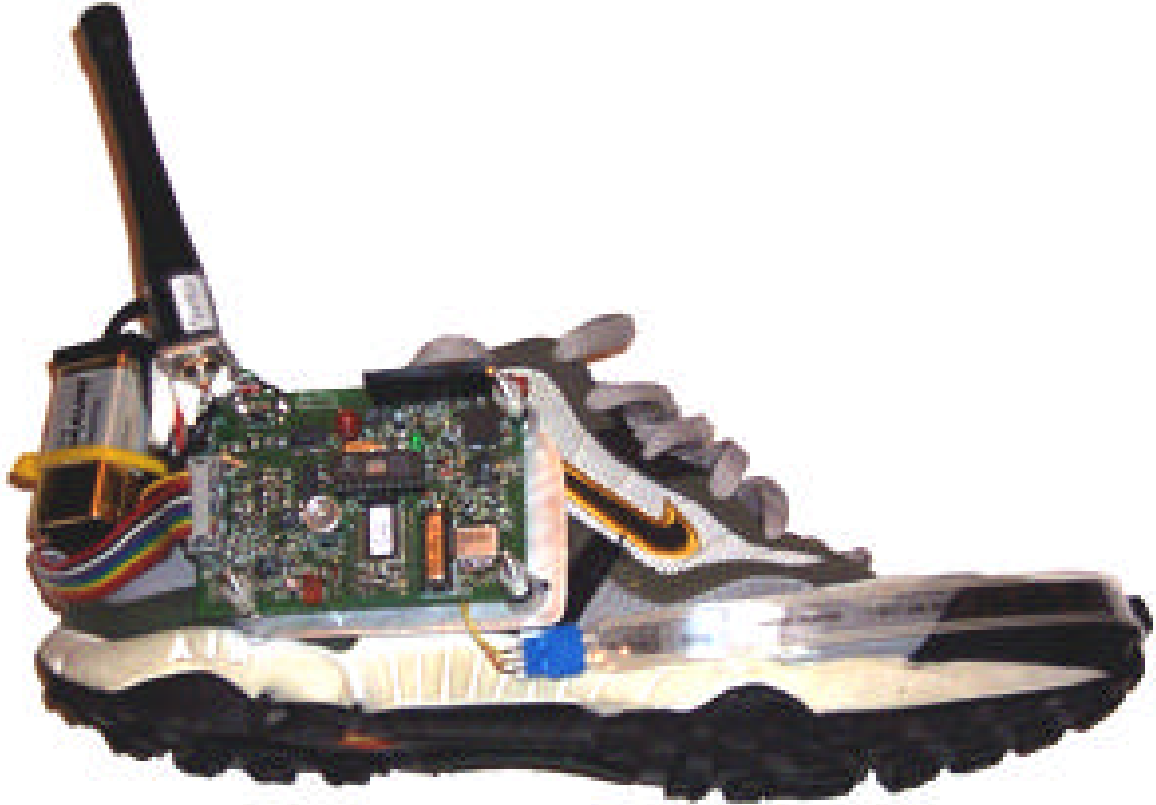
Figure 4: The modern, perfected shoe, with protective electronics cover removed
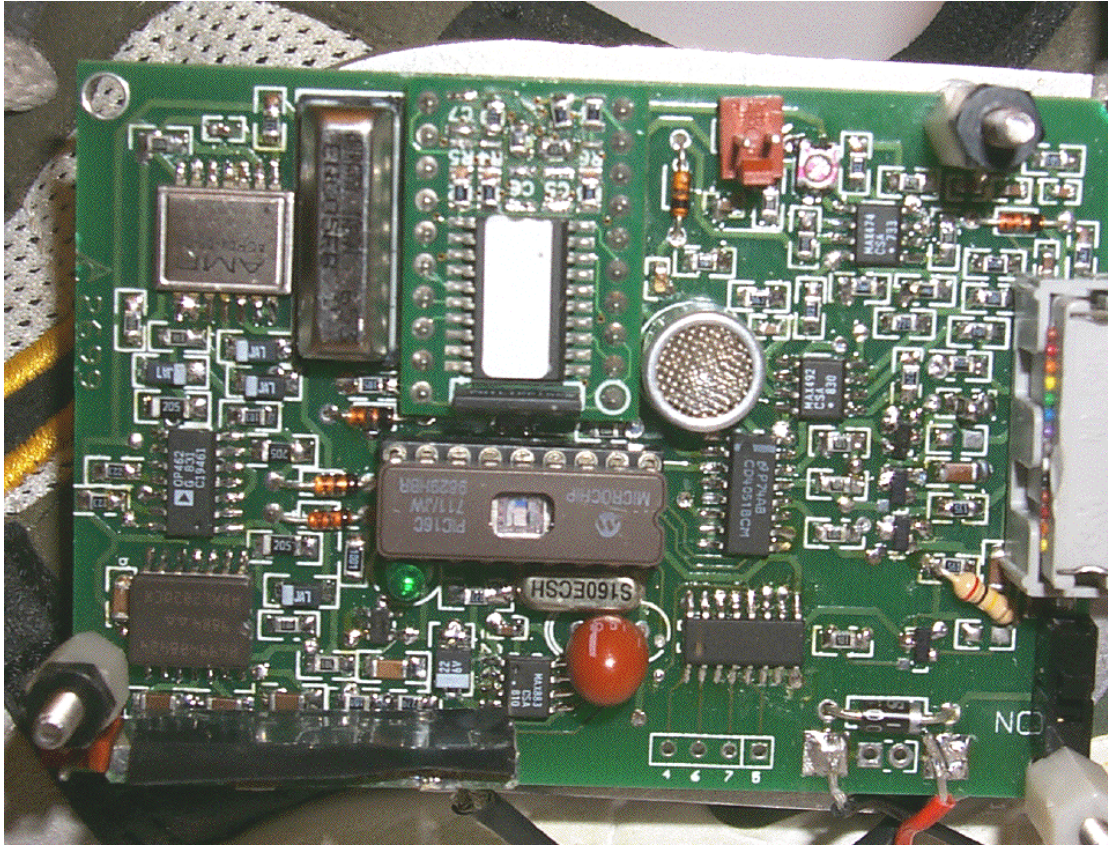
Figure 5: A close-up of the most recent sensor circuit card
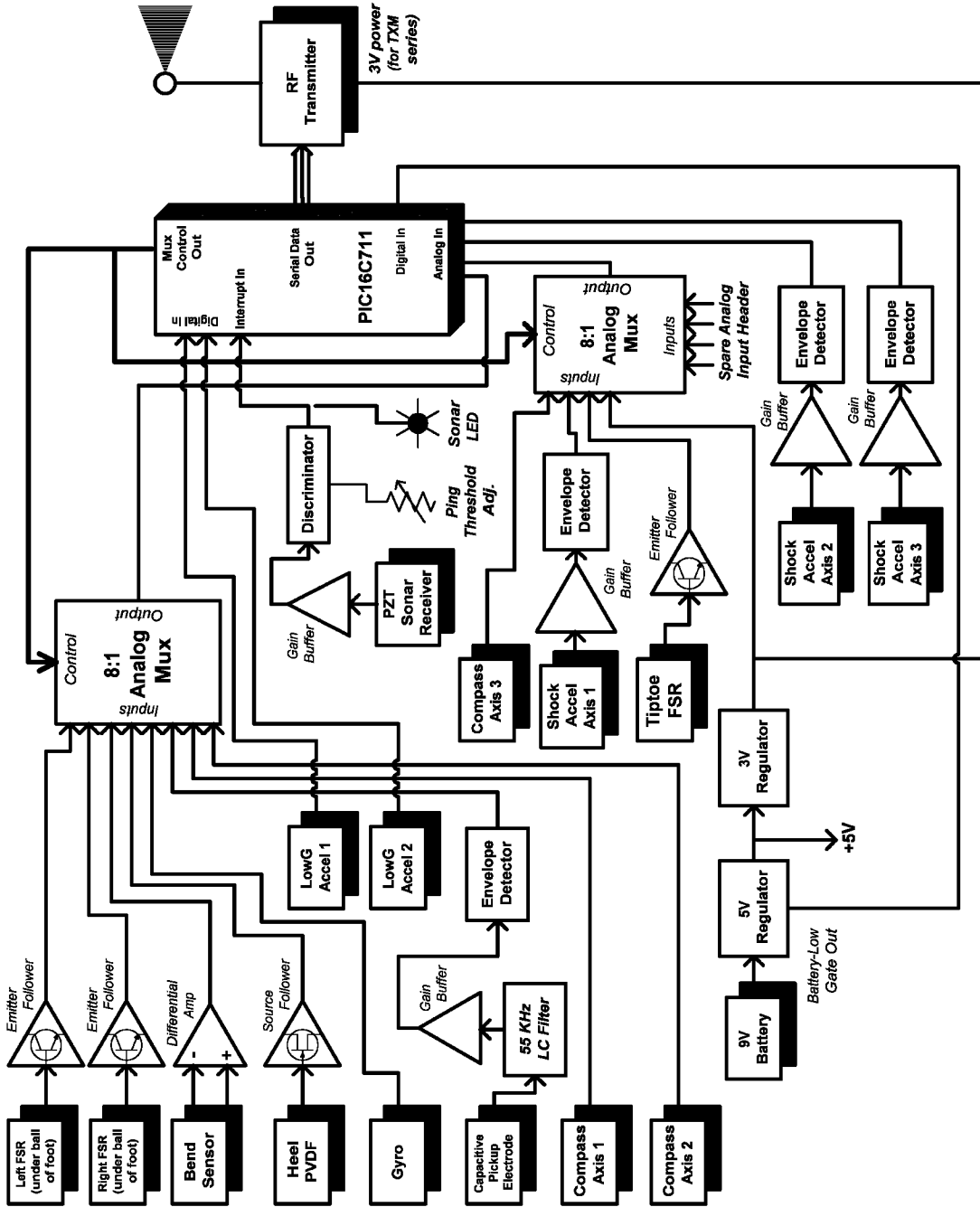
Figure 6: Block Diagram for the shoe-mounted circuitry
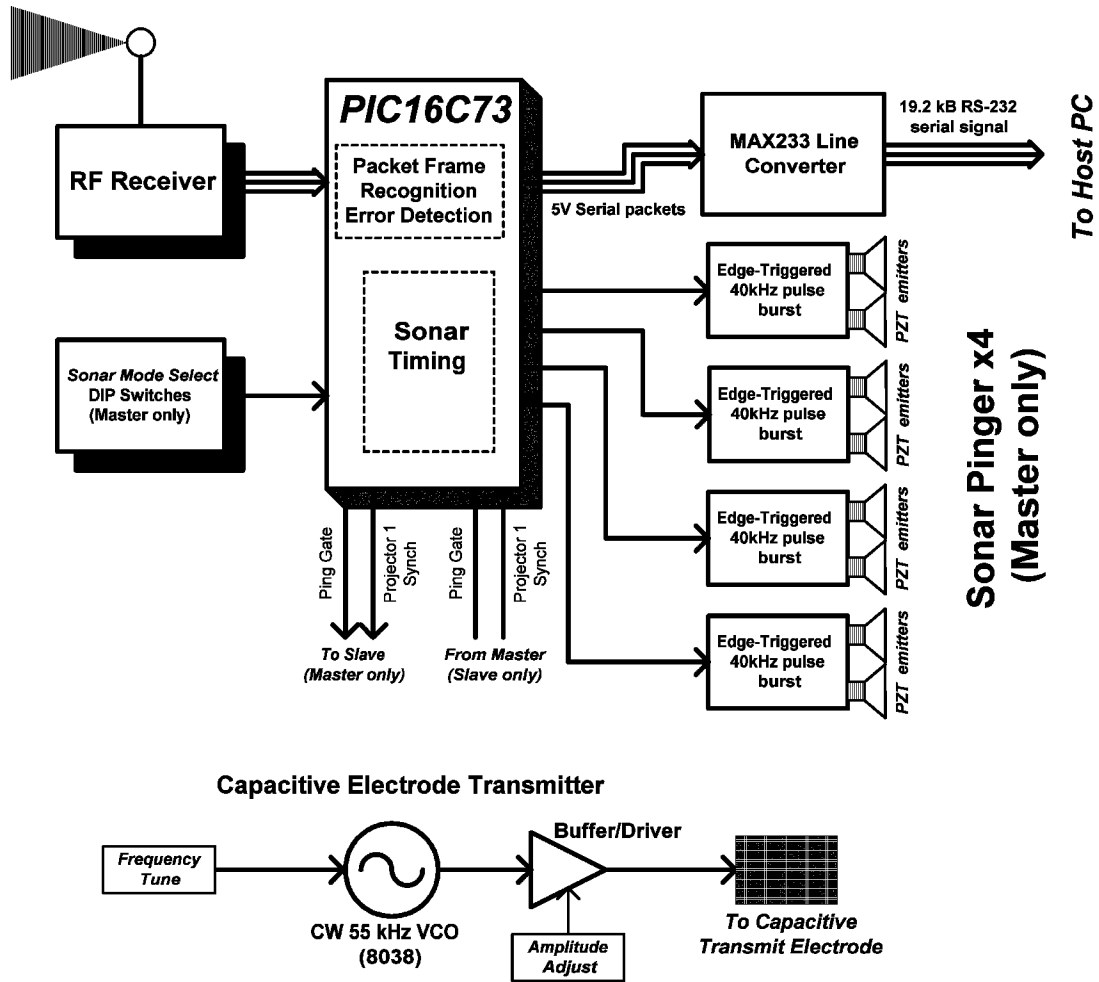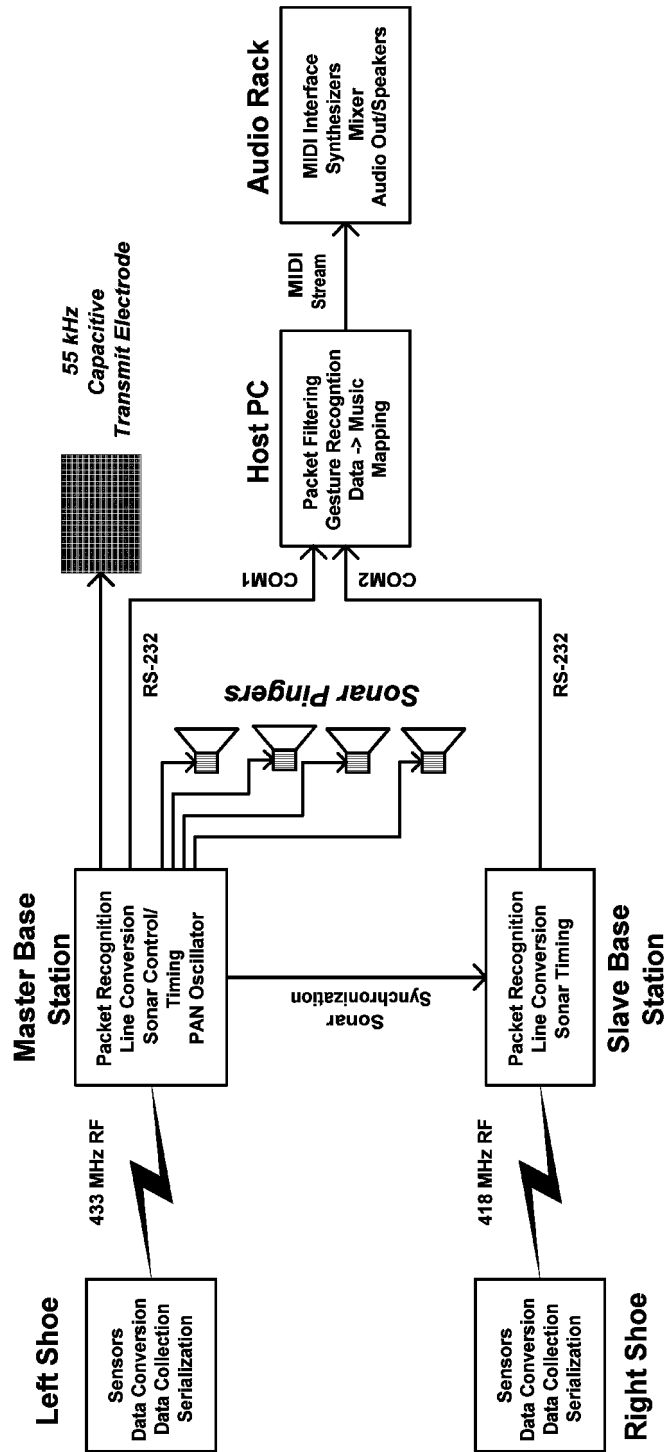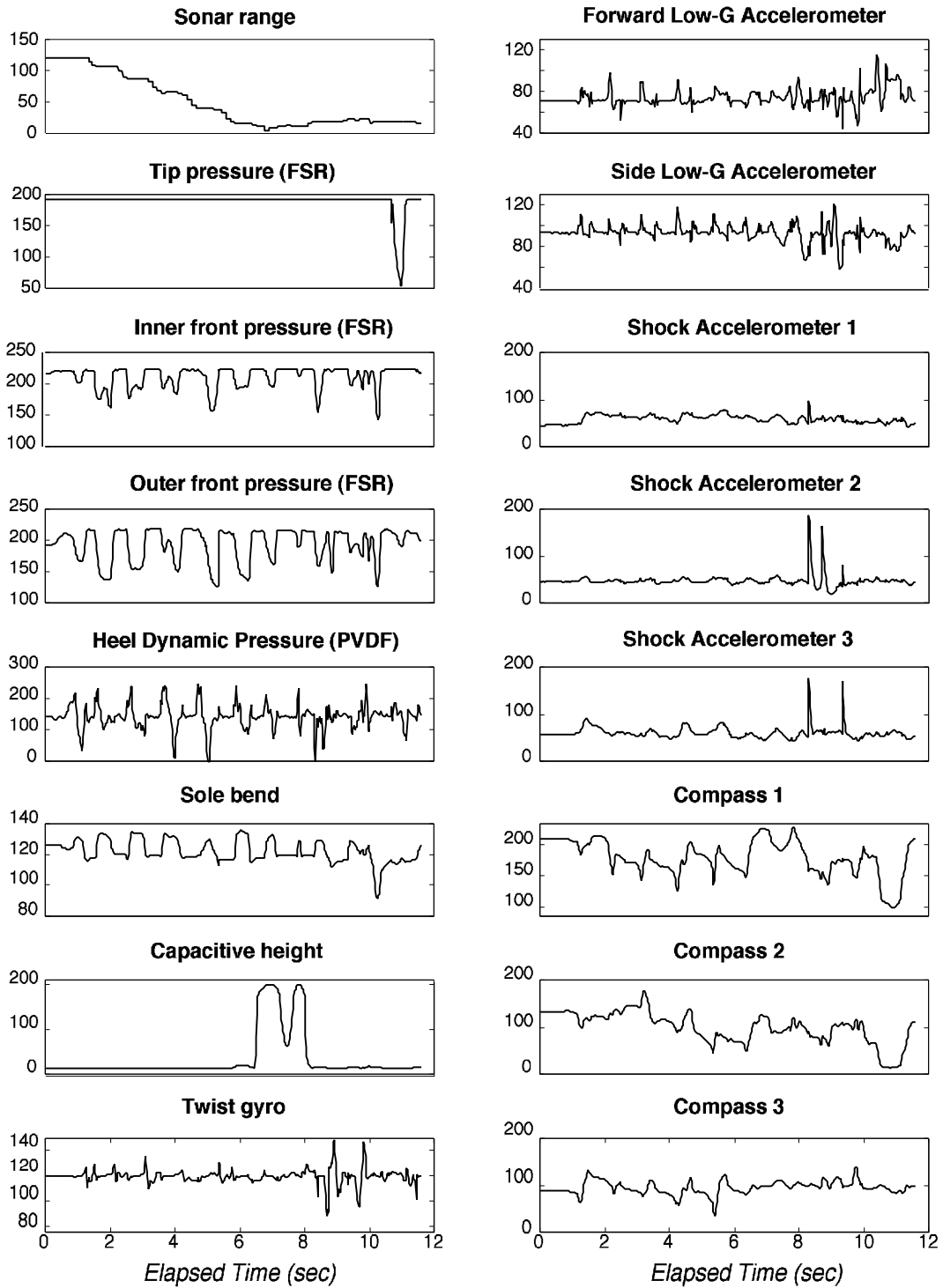
Figure 7: Block diagram for a basestation

Figure 8: Configuration of the fully-deployed Expressive Footwear System

Figure 9: A sample segment of data showing the response of all shoe sensors

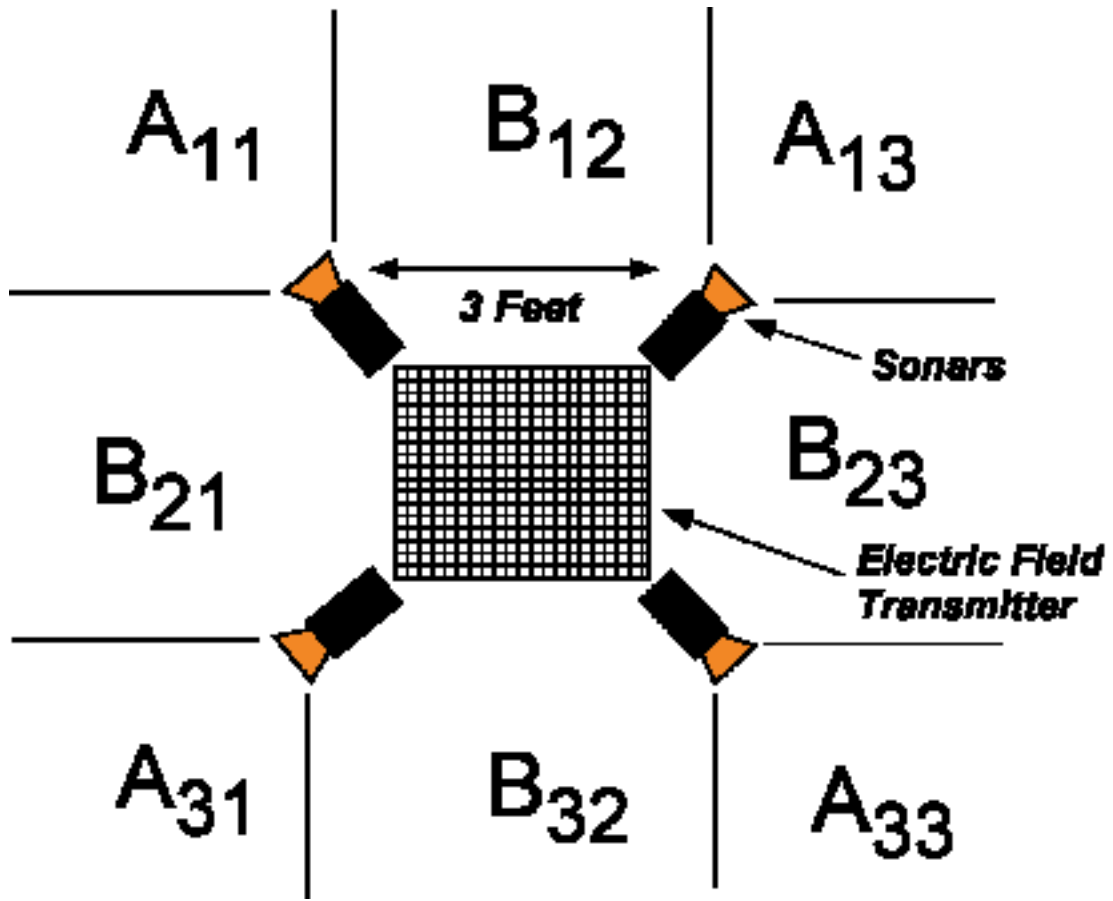**Figure 10: A photo gallery of expressive footwear interactive music projects**

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Figure 11: Layout of the stage (overhead view) for the American Dance Festival and Sens*bles 1999 Performances

Figure 12: Recent collaborations with the Synthetic Characters Group using Expressive Footwear technology: the "chicken" interface for *SWAMPED!* and the IMU bread bun for *Void*
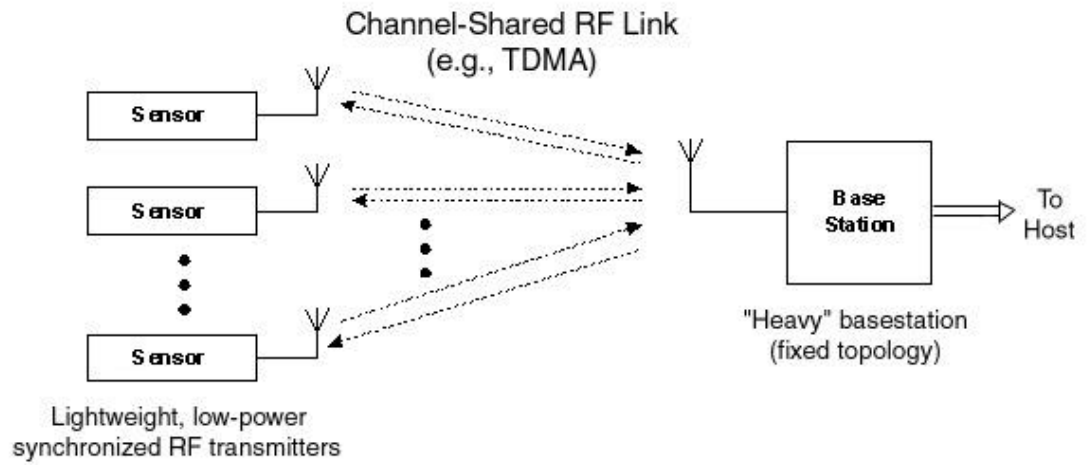
Figure 13: Channel-Shared asymmetric RF network now under development for the next-generation of dense wireless sensing performance projects